

*Complex Baseband Representation of
Real Band-pass Signals: Main Result*

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- Title dissection
 - Representation
 - * $x(t)$: a time function
 - * $X(f) \triangleq \mathcal{F}\{x(t)\}$: a frequency domain representation of $x(t)$
 - Complex baseband signal $\stackrel{?}{\equiv}$ real bandpass signal
 - In what sense?

- Why **real bandpass** signals and systems do we deal with?

- What is the advantage of handling **complex baseband** representation of real bandpass signals and systems?

- Why real bandpass signals?

- Electrical signals are real-valued.

- $\left\{ \begin{array}{l} \text{current} \\ \text{voltage} \end{array} \right.$

- Fig.

- In many systems, spectrum is a valuable resource. For example, in a cable for CATV, we want to put as many channel signals as possible.
- Fig.

- What is the advantage of handling complex baseband signals instead of real bandpass signals?
 - Two real numbers are equivalent to one complex number
 - * There are many cases where handling a complex number is much easier than handling two real numbers.

– In real bandpass signaling, it can be shown that two real baseband signals contain “all” the information of the real bandpass signal

$$\begin{array}{ccccccc}
 x(t) & \equiv & (x_c(t), x_s(t)) & \equiv & z(t) \triangleq & x_c(t) + jx_s(t) \\
 \text{one real bandpass} & & \text{two real baseband} & & \text{one complex baseband}
 \end{array}$$

- The main result
 - Given
 - * $x(t)$, a real-valued “bandpass” signal with finite energy and
 - * $X(f) \triangleq \mathcal{F}\{x(t)\}$ that has a finite support $f \in (0, B]$,
 - we choose $f_c \in (B/2, B)$ and $\theta \in [0, 2\pi)$. (← NOT unique!)
 - Then, there **exists** a unique pair $x_c(t)$ and $x_s(t)$ of real-valued band-limited **baseband** signals such that

$$\begin{aligned}
 x(t) &= x_c(t) \cos(2\pi f_c t + \theta) - x_s(t) \sin(2\pi f_c t + \theta) \\
 &= \operatorname{Re}\{(x_c(t) + jx_s(t))e^{j(2\pi f_c t + \theta)}\}
 \end{aligned}$$

where $j \triangleq \sqrt{-1}$.

$$- e^{j\phi} = \cos \phi + j \sin \phi \quad (\text{Euler's identity})$$

- $x_c(t) \cos(2\pi f_c t + \theta)$: in-phase component of $x(t)$
– $x_s(t) \sin(2\pi f_c t + \theta)$: quadrature component of $x(t)$. ($2\pi/4 = 90^\circ$)
- The complex baseband signal $x_c(t) + jx_s(t)$, the center frequency f_c , and the phase θ contain all the information carried by $x(t)$.
- The complex baseband signal $x_c(t) + jx_s(t)$ is called **the complex envelope** of the real bandpass signal $x(t)$ and often denoted by $x_l(t)$.
- $x_c(t)$: real part of $x_l(t)$. Often called the in-phase component of $x_l(t)$
 $x_s(t)$: imaginary part of $x_l(t)$. Often called the quadrature component of $x_l(t)$.

- It is obvious that,
if $x_c(t)$ and $x_s(t)$ are real-valued baseband signals having bandwidth B' ,
then $x(t) \triangleq x_c(t) \cos(2\pi f_c t + \theta) - x_s(t) \sin(2\pi f_c t + \theta)$ is a real-valued bandpass signal for $f_c > B'$.

- The main result says that a kind of the converse of this statement is also true.
- How can we prove?
 - * In the time domain, we have no idea.
We tackle the problem in the frequency domain.