

EEEE 695F Fall 05
HW#2

(5) 1. Answer the following questions

(a) Show that any real-valued function $f(t)$ can be written as

$$f(t) = f_e(t) + f_o(t) \quad \text{called the odd part}$$

where $f_e(t) = f_e(-t)$ and $f_o(t) = -f_o(-t)$
the even part

(b) Show that any real-valued square matrix C can be written as

$$C = S + A \quad \text{called the anti-symmetric part.}$$

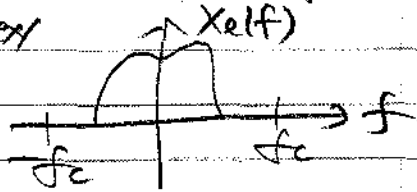
where $S = S^T$ and $A = -A^T$
called the symmetric part

(5) 2. Suppose that your receiver can coherently demodulate the signal. Discuss why in this case you prefer SSB (single-side band) modulation over DSB (double side band) for AM radio broadcasting?

(5) 3. Design a system that has a real bandpass signal $x(t) = \text{Re}\{x_e(t)e^{j2\pi f_c t}\}$ as the input and the envelope $|x_e(t)|$ as the output. All your components must have real inputs & real outputs.

(5) 4 Answer the following questions.

Assume $x(t)$ & $h(t)$ are complex baseband signals with bandwidth less than f_c .



(a) Show that

$$(h(t) e^{j2\pi f_c t}) * (x(t)^* e^{-j2\pi f_c t}) = 0, \quad \forall t$$

(b) Show that

$$\begin{aligned} (h(t) e^{j2\pi f_c t}) * (x(t) e^{j2\pi f_c t}) \\ = (h(t) * x(t)) e^{j2\pi f_c t} \end{aligned}$$

(5) 5 Answer the following questions

Assume that $f(t)$ & $g(t)$ are real-valued baseband signals w/ bandwidth less than f_c .

(a) Show that

$$f(t) \cos(2\pi f_c t + \theta) = \operatorname{Re}\{(f(t) e^{j\theta}) e^{j2\pi f_c t}\}$$

(b) Show that

$$\int_{-\infty}^{\infty} f(t-\tau) g(\tau) \cos 2\pi f_c (t-2\tau) d\tau = 0$$

$\forall t$

(20) 6 The received signal is modeled as

$$y(t) = \text{Re} \{ g(t) e^{j2\pi f_c t} \}$$

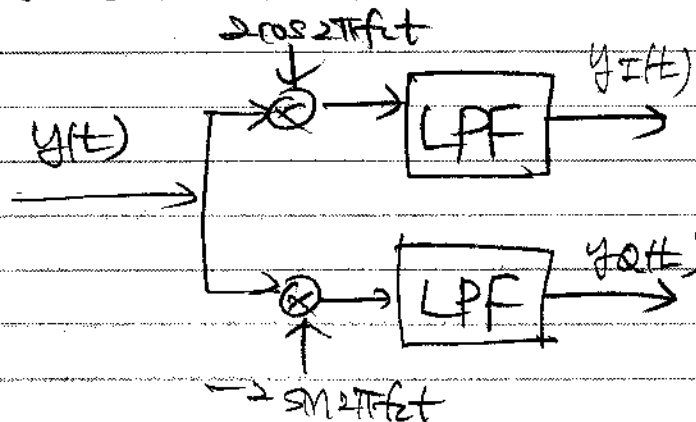
where $g(t)$ is a complex baseband signal w/ bandwidth less than f_c .

We want to correlated the complex envelope $g(t)$ with a complex signal $f_c(t) \triangleq f_I(t) + j f_Q(t)$

in the baseband, i.e., we want to design a system that down-converts $y(t)$ and then perform

$$\int_{-\infty}^{\infty} y(t) f_c(t)^* dt$$

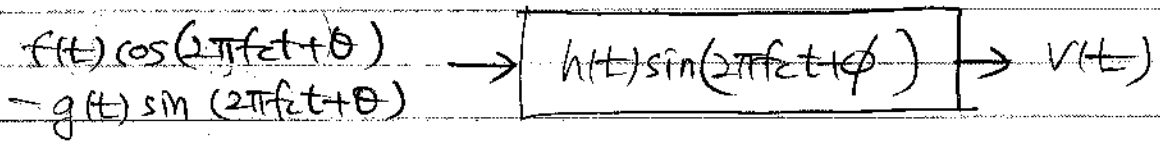
However, we are restricted to use real-input/real-output systems only and to use the I-Q demodulator:



Draw a block diagram that processes $y_I(t)$ & $y_Q(t)$.

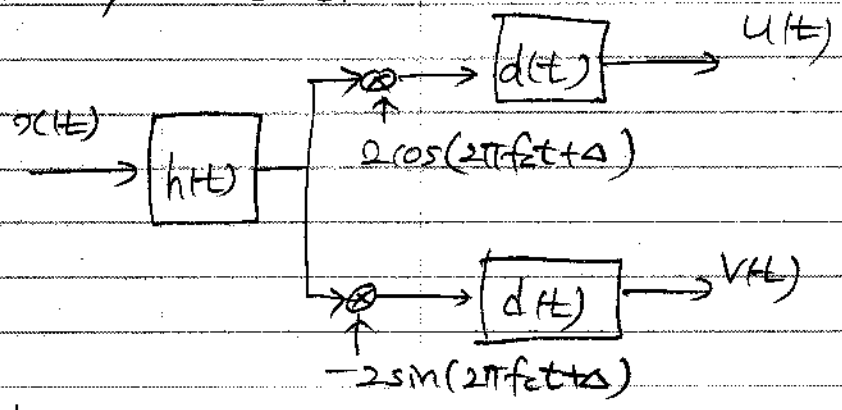
(5) 7. Suppose that $f(t)$, $g(t)$, and $h(t)$ are all real-valued baseband signals with bandwidth $< f_c$.

Find the output $v(t)$ of the following system.



(5) 8. Suppose that $a(t)$, $b(t)$, $c(t)$, and $d(t)$ are all real-valued baseband signals w/ bandwidth less than f_c .

Find the output $u(t)$ & $v(t)$ of the following homodyne receiver.



where

$$x(t) = a(t) \cos(2\pi f_c t + \theta) - b(t) \sin(2\pi f_c t + \theta)$$

and

$$h(t) = 2c(t) \sin(2\pi f_c t - \phi)$$

(5) 9. Let $x(t)$ be a real-valued bandpass signal w/ energy E . Find the energy of the complex envelope $x_e(t)$.