

Review of Handout #13

- o ✓ The Most popular OFDM signal model

$$X(t) = \sum_{k=1}^K X_k e^{j2\pi f_k t}, \quad 0 \leq t < T_0$$

where

$$f_{k+1} - f_k = \frac{1}{T_0}, \quad \forall k$$

← To keep the orthogonality

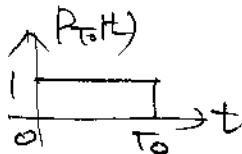
⇒ No PSD because $X(t)$ is not a power signal

- o Slight modification of the most popular model

$$X(t) = \sum_{k=1}^K \left(\sum_{m=-\infty}^{\infty} X_k[m] P_{T_0}(t - mT_0) \right) e^{j2\pi f_k t},$$

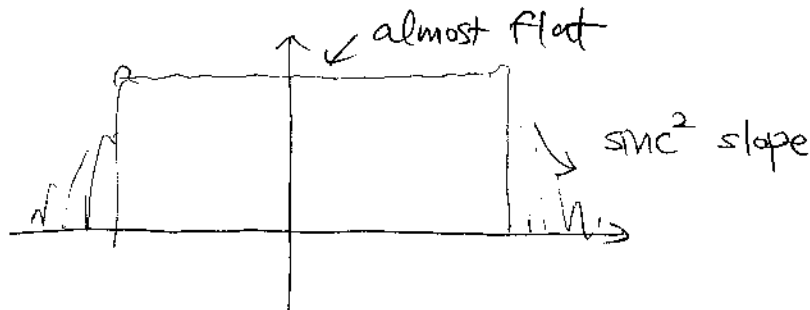
, $-\infty < t < \infty$ assume uncorrelated w/ unit power

where



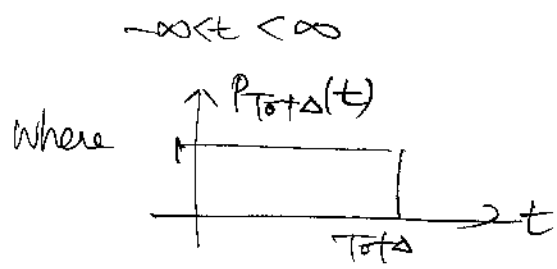
and $f_{k+1} - f_k = \frac{1}{T_0}, \quad \forall k$

$$\Rightarrow S_{XX}(f) = \sum_{k=1}^K \frac{1}{T_0} \left(P_{T_0}(f - f_k) \right)^2 \propto \sum_{k=1}^K \frac{1}{T_0} \text{sinc}^2((f - f_k)T_0)$$



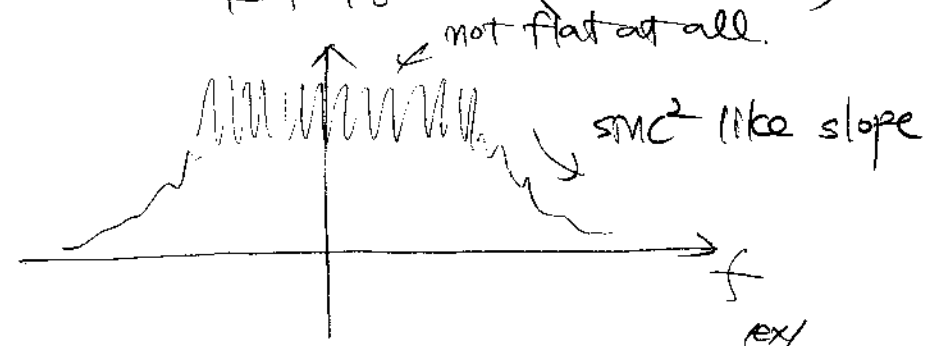
- o More modification to adopt CP (Cyclic Prefix)

$$X(f) = \sum_{k=1}^K \left(\sum_{m=-\infty}^{\infty} X_k(m) P_{\text{Total}}(t - m(T_{\text{Total}})) \right) e^{j2\pi fct}$$

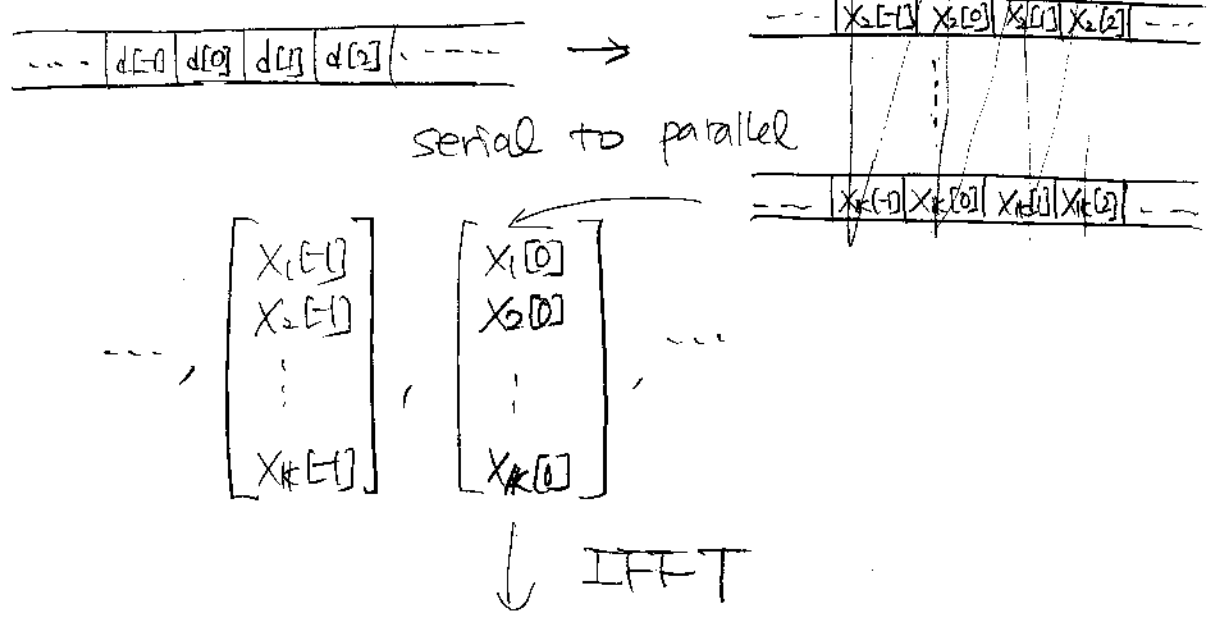


and $f_{k+1} - f_k = \frac{1}{T_0} \cdot \frac{1}{K}$

$$\Rightarrow S_{XX}(f) \propto \sum_{k=1}^K \frac{1}{T_0} \text{sinc}^2((f - f_k)(T_{\text{Total}}))$$

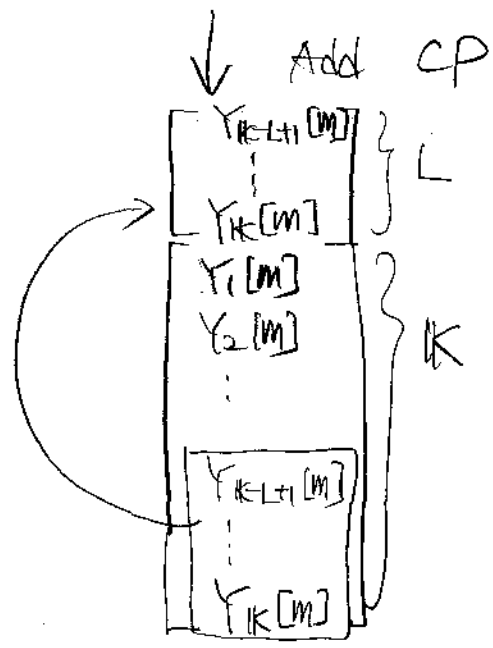


o IFFT-based OFDM

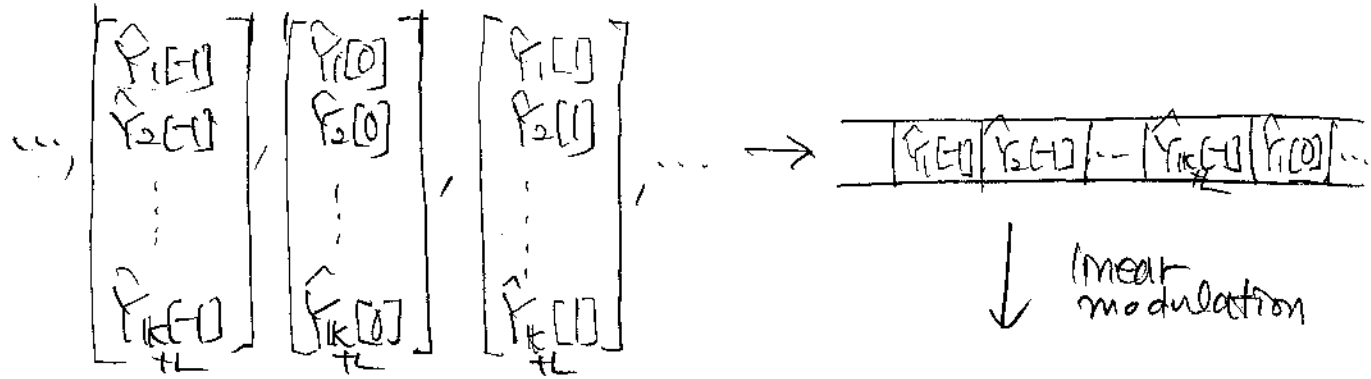


$$Y[M] = \text{IFFT } X[M]$$

$$= X_1 \begin{bmatrix} \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot 0 \cdot 0} \\ \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot 0 \cdot 1} \\ \vdots \\ \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot 0 \cdot (K-1)} \end{bmatrix} + \dots + X_K \begin{bmatrix} \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot (K-1) \cdot 0} \\ \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot (K-1) \cdot 1} \\ \vdots \\ \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K} \cdot (K-1) \cdot (K-1)} \end{bmatrix}$$



↓ parallel to serial conversion



$$\begin{aligned}
 X(t) &= \sum_{m=-\infty}^{\infty} \left(\sum_{k=1}^{K+L} Y_k[m] p(t - (k + (k+L))T_c) \right) \quad 4 \\
 &= \sum_{m=-\infty}^{\infty} \sum_{k=1}^{K+L} \left(\sum_{k'=1}^{K+L} X_{k'}[m] \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K}(k-L)(k'-1)} \right) \times \\
 &\quad p(t - (k + (k+L))mT_c) \\
 &= \sum_{m=-\infty}^{\infty} \sum_{k'=1}^{K+L} X_{k'}[m] \left(\sum_{k=1}^{K+L} \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K}(k-L)(k'-1)} \times p(t - (k + (k+L))mT_c) \right) \\
 &\quad \cong S_{k'}(t - m(K+L)T_c) \\
 &= \sum_{k'=1}^{K+L} \left(\sum_{m=-\infty}^{\infty} X_{k'}[m] S_{k'}(t - mT_b) \right)
 \end{aligned}$$

where $T_b = (K+L)T_c$

linearly modulated signal w/
Tx pulse $s_k(t)$ & symbol time T_b .

$$\Rightarrow S_{XX}(f) = \sum_{k'=1}^{K+L} \frac{1}{T_b} |S_{k'}(f)|^2 \quad \text{assuming uncorrelated data seq. w/ unit power}$$

$$= \sum_{k'=1}^{K+L} \frac{1}{T_b} |P(f)|^2 \left| \sum_{k=1}^{K+L} \frac{1}{\sqrt{K}} e^{j\frac{2\pi}{K}(k-L)(k'-1)} \times e^{-j2\pi f k T_c} \right|^2$$

$$\cong \sum_{k'=1}^{K+L} \frac{1}{T_b} |P(f)|^2 \times e^{j2\pi k(fT_c - \frac{k-L}{K})}$$

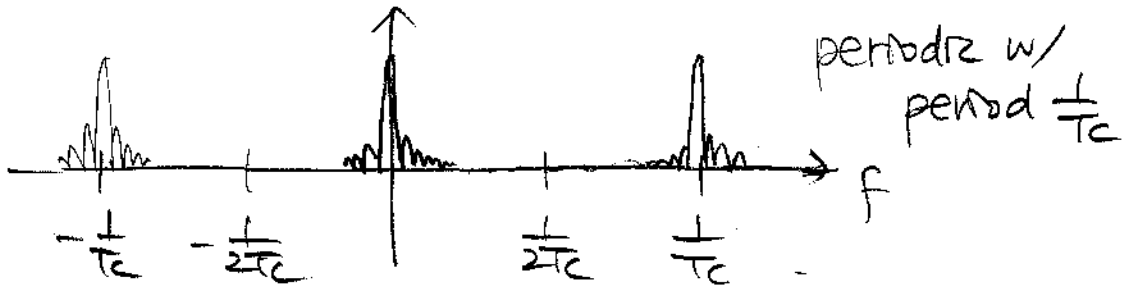
DTFT of a finite-support DT signal evaluated at fT_c

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where

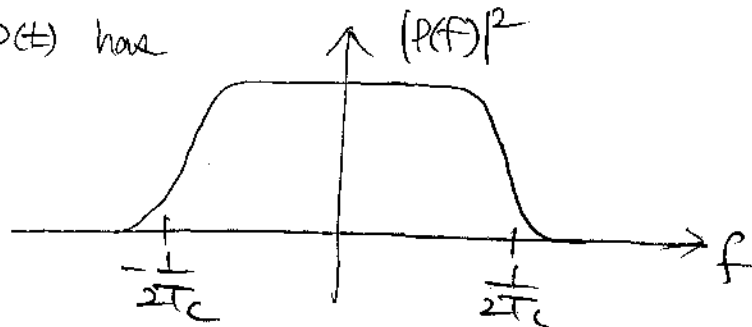
$$W(f) \Rightarrow \left| \sum_{k=0}^{K+L-1} \frac{1}{\sqrt{K}} e^{j2\pi f k T_c} \right|^2$$

$$= \left| \frac{\sin(\pi f (K+L) T_c)}{\sin(\pi f T_c)} \right|^2$$



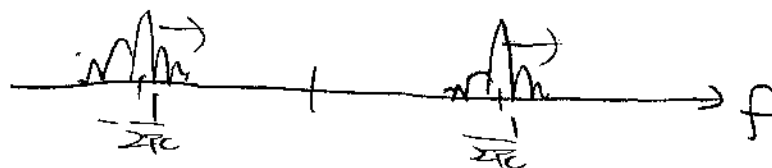
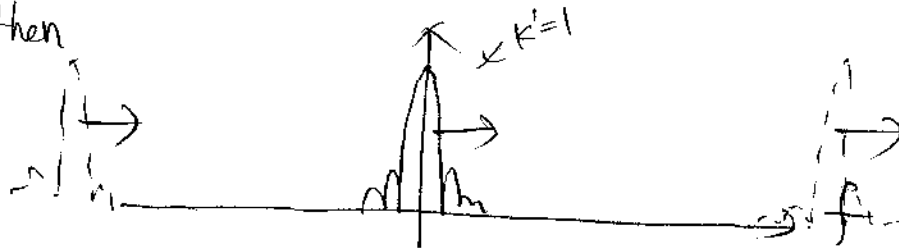
o Null sub-carriers

If $P(f)$ has

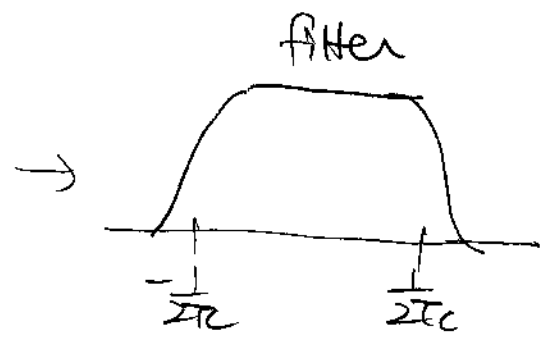
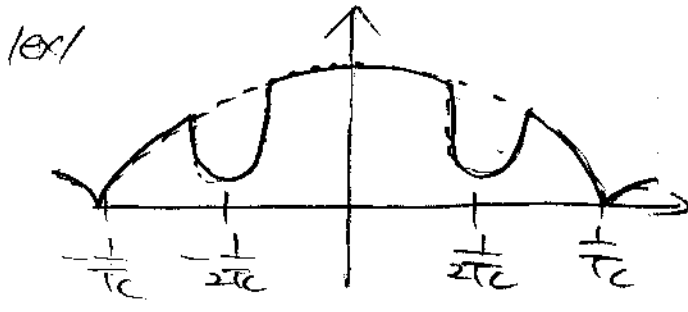
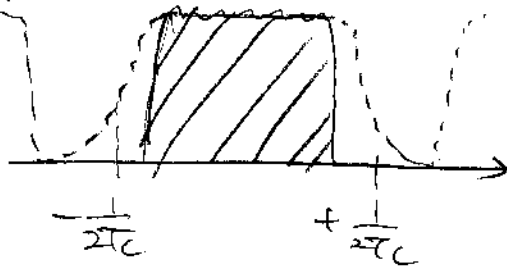


and uncorrelated $X(n)$,

then



To make this spectrum as similar as that of modified w/ rectangular... we put null subcarriers so that



$\Rightarrow K$: # of FFT points
 N : # of null subcarriers.

$\Rightarrow K - N$ subcarriers

Review of PAM & the optimal [↑] front end. continuous-time

○ Review of PAM (received signal model)

① Real baseband signal model

$$z(t) = \sqrt{P} \sum_{m=-\infty}^{\infty} d[m] p(t-mT) + N(t)$$

where P is the signal power

$$E\{d[m]\} = 0, \quad E\{d[m]^2\} = 1,$$

$$\|p(t)\|^2 = T,$$

$N(t)$ is a real-valued AWGN w/ $S_{NN}(f) = \frac{N_0}{2}$

② Real passband signal model

$$z(t) = \text{Re}\left\{ \sqrt{2P} \sum_{m=-\infty}^{\infty} d[m] p(t-mT) e^{j2\pi f_c t} \right\} + N(t)$$

where P is the signal power

$$E\{d[m]\} = 0, \quad \begin{cases} E\{d[m]^2\} = 1 & \text{(for BPSK)} \\ E\{d[m]^2\} = 0, \quad E\{|d[m]|^2\} = 1 \end{cases}$$

$$\|p(t)\|^2 = T,$$

$N(t)$ is a real-valued AWGN w/ $S_{NN}(f) = \frac{N_0}{2}$

③ Complex baseband signal model I

$$z_c(t) = \sqrt{2P} \sum_{m=-\infty}^{\infty} d[m] p(t-mT) + N_c(t)$$

where $(*)$, $(**)$, $(***)$, and

$N_c(t)$ is a proper-complex AWGN w/ $S_{N_c N_c}(f) = 2N_0$

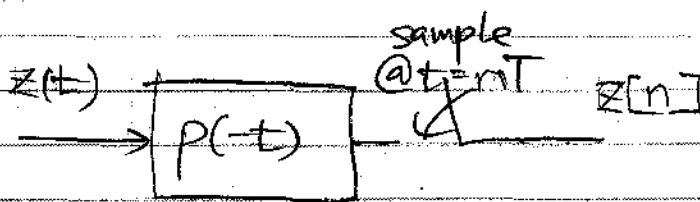
② Complex baseband signal model II

$$z_c(t) = \sqrt{P} \sum_{m=-\infty}^{\infty} d[m] p(t-mT) + N_c(t)$$

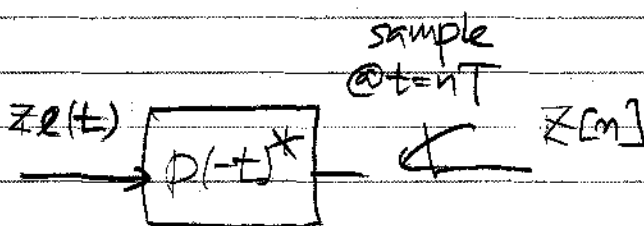
where $(*)$, $(**)$, $(***)$, and $N_c(t)$ is a proper-complex AWGN w/ $S/N_c = N_0$

① Review of PAM (optimal receiver front end)

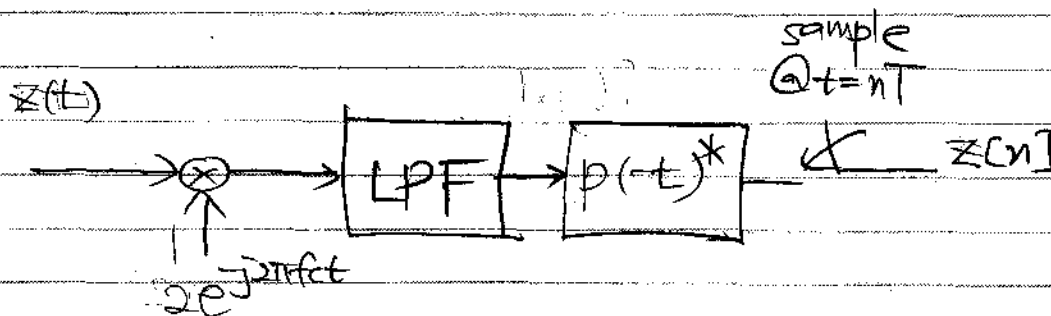
① Real baseband case



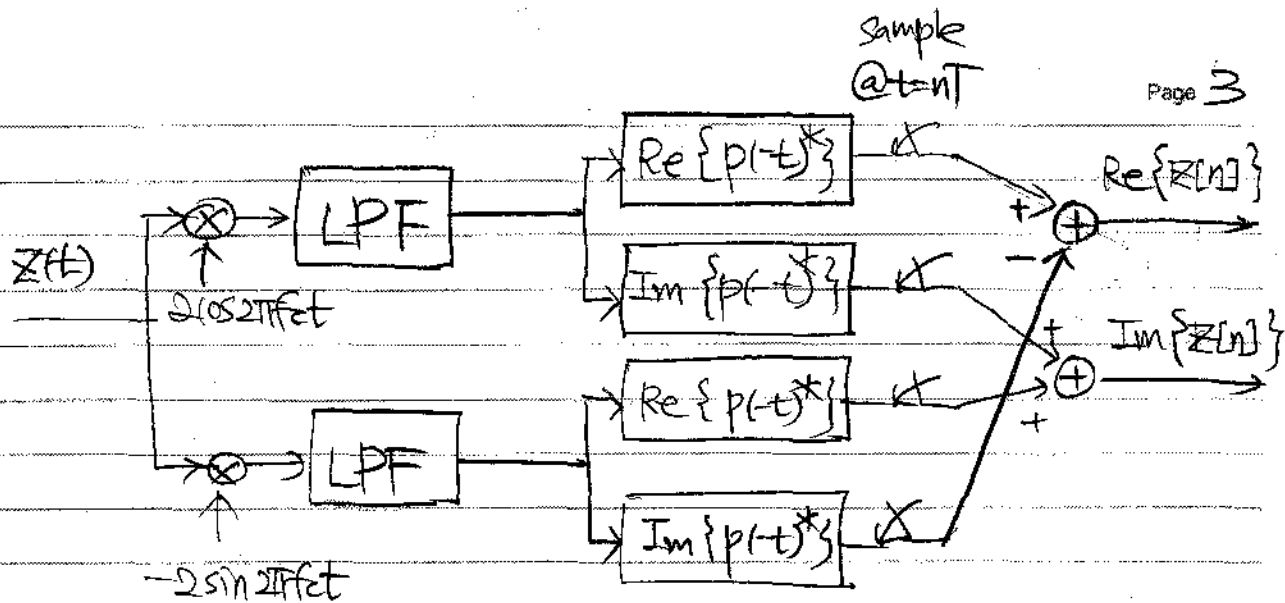
② Complex baseband case



③ Real passband case

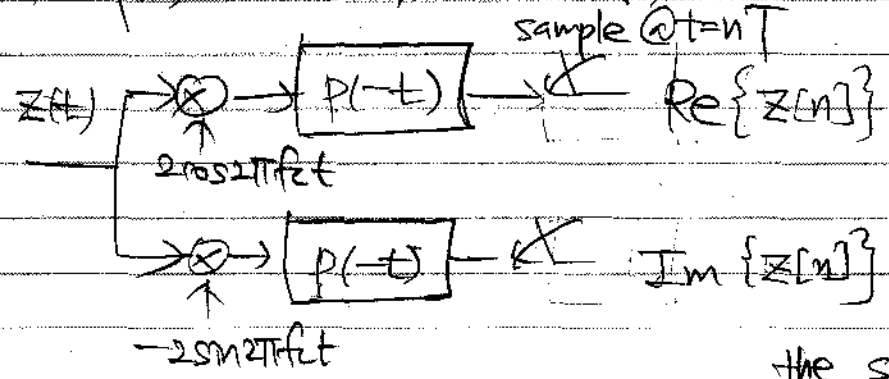


complex I-Q demodulator



real I-Q demodulator

• If $p(t)$ is real, baseband



the sufficient statistic

○ Review of the properties of $\{z[n]\}_{n=-\infty}^{\infty}$

$$z[n] = \sqrt{2P} \sum_{m=-\infty}^{\infty} d[m] \int_{-\infty}^{\infty} p(t-mT) p(t-nT)^* dt + \int_{-\infty}^{\infty} N_c(t) p(t-nT)^* dt$$

• Signal component

If we define

$$P(t) \triangleq p(t) * p(-t)^* = p(-t)^* * p(t)$$

then, from

$$\begin{aligned}\tilde{p}(t) &= \int_{-\infty}^{\infty} p(t+\tau) p^*(t-\tau) d\tau \\ &= \int_{-\infty}^{\infty} p(\tau+t) p^*(\tau) d\tau\end{aligned}$$

$$\Rightarrow \int_{-\infty}^{\infty} p(t-mT) p^*(t-nT) dt = \tilde{p}((n-m)T),$$

We obtain

$$\begin{aligned}R_{\tilde{p}}[m] &= \sqrt{2P} \sum_{n=-\infty}^{\infty} d[n] \tilde{p}((n-m)T) + N_e[m] \\ &= \underbrace{\left(\sqrt{2P} d[m] \tilde{p}(0) + \sqrt{2P} \sum_{m \neq n} d[n] \tilde{p}((n-m)T) \right)}_{\text{ISI}} + N_e[m]\end{aligned}$$

• Gaussian noise component

$$\begin{aligned}R_{N_e N_e}[m] &\triangleq E \{ N_e[m] N_e^*[m+m] \} \\ &= E \left\{ \left(\int_{-\infty}^{\infty} N_e(t) p(t-mT) dt \right)^* \int_{-\infty}^{\infty} N_e(t) p(t-(m+m)T) dt \right\} \\ &= 2N_0 \int_{-\infty}^{\infty} p(t-mT) p^*(t-(m+m)T) dt \\ &= \underbrace{2N_0 \tilde{p}(mT)}\end{aligned}$$

In general, this sequence is not proportional to $\delta[m]$. \therefore The noise sequence is colored in general.

- A very special case where $p(t)$ is a square-root Nyquist pulse.

$$\text{If } \tilde{p}(nT) \propto \delta_{n,0}$$

$$\equiv \sum_{m=-\infty}^{\infty} \left| P(f + \frac{m}{T}) \right|^2 = \text{a constant } \forall f$$

← called the **folded spectrum**

then

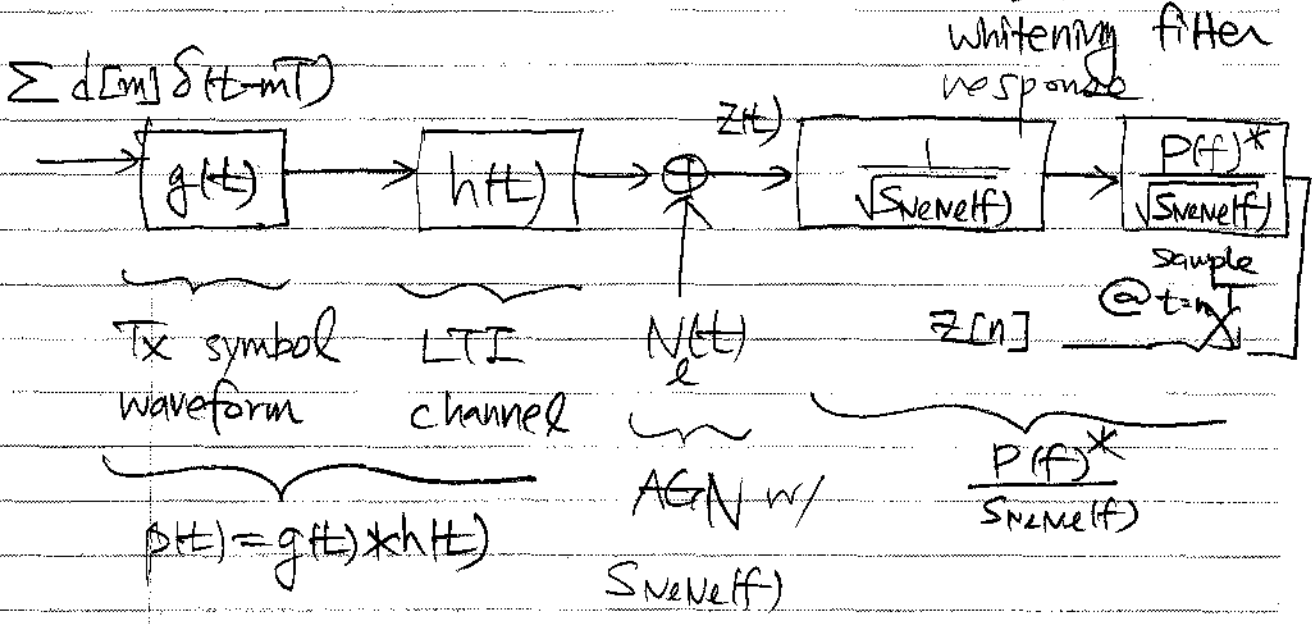
- There is no ISI in the signal component and
- The noise sequence is white.

○ Summary

- For a PAM, the matched filter matched to the symbol waveform and the following baud rate sampling can generate a sequence that is sufficient.
- The sequence contains the ISI and a colored noise component unless the symbol waveform is a square-root Nyquist pulse.
- For the matched filtering, we need to know $p(t)$, which may not be realistic in general because $p(t)$ is usually the convolution of the transmitted symbol waveform $g(t)$ and the channel impulse response $h(t)$, i.e.,

$$p(t) = g(t) * h(t)$$
 and $h(t)$ may not be known to the receiver.

This result is from the AWGN assumption on $N(f)$ or $N_e(f)$. If it is colored, then the noise must be whitened first. Then, the RX filter needs to match to $p(f) * h_w(f)$



In this case, the data sequence has the desired waveform $\int_{-1}^1 \frac{|P(f)|^2}{S_n N_e(f)}$ and the

noise PSD $\propto |P(f)|^2$

Note that if the noise is white then we have $\int_{-1}^1 |P(f)|^2$ and $|P(f)|^2$, respectively.

In the next handout, we only consider the case where the AWGN $N(f)$ or $N_e(f)$ is white, so that the desired waveform and the noise autocorrelation function both of them are proportional to $p(nT)$.