

Image-Band Problem and IR Filter: Revisited

Prof. Joon Ho Cho

Department of Electrical Engineering, POSTECH

- Review. A heterodyne receiver has two LOs,
 - LO_1 used to down-convert an RF signal to an IF, and
 - LO_2 used to down-convert to the baseband.

Before the down-conversion to the IF,

- **an image band** must be rejected by **an IR filter**
- if either interference or noise is present in the image band.

Similar to upper-side tuning and lower-side tuning in heterodyne transmission,

- there are **two LO frequencies** to choose in down-conversion to the IF, and
- there are **two different image bands** in heterodyne reception.

- Preview. The **image-band problem in down-conversion to IF** is revisited. **By using all real-input real-output subsystems**, the problem and IR filtering are explained in the FD.

- Received Signal Model

- The signal $y(t)$ received by an antenna consists in general of a desired signal, interference, and noise.

$$y(t) = \tilde{x}(t) + I(t) + N(t).$$

- Fig. block diagram of Rx front end

- Fig. received signal viewed in FD

- Down-conversion to IF with LO_1 frequency $f_c - f_{\text{IF}}$ and image band centered at $\pm(f_c - 2f_{\text{IF}})$

- We've seen that, in this case, the IF signal is obtained by

$$y_{\text{IF}}(t) = \text{CS}\{\text{IR}(y(t)) \cdot 2 \cos(2\pi(f_c - f_{\text{IF}})t + \phi_1)\}$$

- where the IR and the CS filters have real-valued impulse responses.

- Fig. block diagram

- Let's take a look at the down-conversion operation carefully. Without IR filtering, we perform

$$\text{CS} \left[y(t) \cdot \{ e^{j(2\pi(f_c - f_{\text{IF}})t + \phi_1)} + e^{-j(2\pi(f_c - f_{\text{IF}})t + \phi_1)} \} \right] .$$

- So, in the FD, we have

$$Y_{\text{IF}}(f) = \text{CS} \{ Y(f - (f_c - f_{\text{IF}})) e^{j\phi_1} + Y(f + (f_c - f_{\text{IF}})) e^{-j\phi_1} \} .$$

- Fig. In FD, ...

- Notice that the first term moves
 - * the signal located at $-f_c$ to $-f_{\text{IF}}$,
 - * the signal located at f_c to $2f_c - f_{\text{IF}}$, and
 - * the interference and noise located at $-(f_c - 2f_{\text{IF}})$ moves to f_{IF} .
- Notice that the second term moves
 - * the signal located at f_c to f_{IF} ,
 - * the signal located at $-f_c$ to $-2f_c + f_{\text{IF}}$, and
 - * the interference and noise located at $f_c - 2f_{\text{IF}}$ to $-f_{\text{IF}}$.
- To remove the unwanted signal, interference, and noise,
 - * we have to use an **IR filter** to reject the interference and noise **before mixing**, and
 - * we have to use a **CS filter** to remove the high frequency signal and select the desired channel signal **after mixing**.
 - * The stopband of the IR filter is located at $\pm(f_c - 2f_{\text{IF}})$ and have bandwidth ..., and
 - * the passband of the CS filter is located at $\pm f_{\text{IF}}$ and have bandwidth ...

- The output IF signal is given by

$$y_{\text{IF}}(t) = \text{Re}\{(\tilde{x}_l(t)e^{-j\phi_1})e^{j2\pi f_{\text{IF}}t}\}$$

when there is no in-band noise and all interference are filtered out.

Thus, the complex envelope is $\tilde{x}_l(t)e^{-j\phi_1}$.

- The quadrature demodulation paired with this IF down-conversion is given by the real and the imaginary parts of

$$\tilde{x}_l(t)e^{-j(\phi_1+\phi_2)} = \text{LPF} \left[y_{\text{IF}}(t) \cdot 2e^{-j(2\pi f_{\text{IF}}t+\phi_2)} \right],$$

i.e.,

$$\text{Re}\{\tilde{x}_l(t)e^{-j(\phi_1+\phi_2)}\} = \text{LPF} [y_{\text{IF}}(t) \cdot 2 \cos(2\pi f_{\text{IF}}t + \phi_2)]$$

and

$$\text{Im}\{\tilde{x}_l(t)e^{-j(\phi_1+\phi_2)}\} = \text{LPF} [y_{\text{IF}}(t) \cdot (-2 \sin(2\pi f_{\text{IF}}t + \phi_2))].$$

- Fig.

- Down-conversion to IF with LO_1 frequency $f_c + f_{\text{IF}}$ and image band centered at $\pm(f_c + 2f_{\text{IF}})$

- We've seen that, in this case, the IF signal is obtained by

$$y_{\text{IF}}(t) = \text{CS}\{\text{IR}(y(t)) \cdot 2 \cos(2\pi(f_c + f_{\text{IF}})t + \phi_1)\}$$

- where the IR and the CS filters have real-valued impulse responses.

- Fig. block diagram

- Let's take a look at the down-conversion operation carefully. Without IR filtering, we perform

$$\text{CS} \left[y(t) \cdot \{e^{j(2\pi(f_c+f_{\text{IF}})t+\phi_1)} + e^{-j(2\pi(f_c+f_{\text{IF}})t+\phi_1)}\} \right] .$$

- So, in the FD, we have

$$Y_{\text{IF}}(f) = \text{CS}\{Y(f - (f_c + f_{\text{IF}}))e^{j\phi_1} + Y(f + (f_c + f_{\text{IF}}))e^{-j\phi_1}\}.$$

- Fig. In FD, ...

- Notice that the first term moves
 - * the signal located at $-f_c$ to f_{IF} ,
 - * the signal located at f_c to $2f_c + f_{\text{IF}}$, and
 - * the interference and noise located at $-(f_c + 2f_{\text{IF}})$ moves to $-f_{\text{IF}}$.
- Notice that the second term moves
 - * the signal located at f_c to $-f_{\text{IF}}$,
 - * the signal located at $-f_c$ to $-2f_c - f_{\text{IF}}$, and
 - * the interference and noise located at $f_c + 2f_{\text{IF}}$ to f_{IF} .
- To remove the unwanted signal, interference, and noise,
 - * we have to use an **IR filter** to reject the interference and noise **before mixing**, and
 - * we have to use a **CS filter** to remove the high frequency signal and select the desired channel signal **after mixing**.
 - * The stopband of the IR filter is located at $\pm(f_c + 2f_{\text{IF}})$ and have bandwidth ...
 - * The passband of the CS filter is located at $\pm f_{\text{IF}}$ and have bandwidth ...

- The output IF signal is given by

$$y_{\text{IF}}(t) = \text{Re}\{(\tilde{x}_l(t)e^{-j\phi_1})e^{-j2\pi f_{\text{IF}}t}\} = \text{Re}\{(\tilde{x}_l^*(t)e^{j\phi_1})e^{j2\pi f_{\text{IF}}t}\}$$

when there is no in-band noise. Thus, the complex envelope is $\tilde{x}_l^*(t)e^{j\phi_1}$.

- The quadrature demodulation paired with this IF down-conversion is given by

$$\text{Re}\{\tilde{x}_l(t)e^{-j(\phi_1-\phi_2)}\} = \text{LPF}[y_{\text{IF}}(t) \cdot 2 \cos(2\pi f_{\text{IF}}t + \phi_2)]$$

and

$$\text{Im}\{\tilde{x}_l(t)e^{-j(\phi_1-\phi_2)}\} = \text{LPF}[y_{\text{IF}}(t) \cdot 2 \sin(2\pi f_{\text{IF}}t + \phi_2)].$$

- Fig.